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# A NEW TEST OPERATOR, VJ, BASED ON CLASS FREQUENCIES

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WALODDI WEIBULL

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### **FOREWORD**

The research work reported herein was conducted by Prof. Dr. Waloddi Weibull, Chemin Fontanettaz 15, 1012 Lausanne, Switzerland under USAF Contract No. F44620-72-C-0028. This contract, which was initiated under Project No. 7451, "Metallic Materials", Task No. 735106, "Behavior of Metals", was administered by the European Office, Office of Aerospace Research. The work was monitored by the Metals and Ceramics Division, Air Force Materials Laboratory, Air Force Systems Command, Wright-Patterson Air Force Base, Ohio under the direction of Mr. W. J. Trapp, AFML/LL.

This report covers work conducted during the period 1 February 1971 to 30 April 1972. The manusscript was submitted for publication by the author in May 1972.

This technical report has been reviewed and is approved.

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Actg Asst for Reliability Metals and Ceramics Division Air Force Materials Laboratory

### **ABSTRACT**

The test statistic X<sup>2</sup> of the Chi-square test may, if applied to a proper sample, be used for selecting distribution functions. When examining its use for this purpose its decision power was found to be very small due to a kind of pooling, an inherent property of its definition. In order to eliminate this pooling, a new test statistic, denoted by VJ, was introduced. It is defined by the number v. of sample elements which fall within each of r properly defined classes into which the space of the variable x has been divided. In fact X<sup>2</sup> may be regarded as a statistic obtained from VJ by a pooling procedure. For this reason VJ was expected to have a much larger decision power than X<sup>2</sup> as was verified by the example that the decision power for a specified case being 6.6% for X<sup>2</sup> was raised to 69.1% for VJ.

The properties of VJ have been thoroughly examined. In particular the class limits yielding the largest decision power have been determined with the result that, in some cases, the decision power was found to be somewhat larger than anyone so far attained.

The statistic VJ can also be used for stating whether a hypothetical distribution is acceptable or not and also for selecting the most probable one within a set of such distributions. Necessary tables for the practical use have been prepared.

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### INTRODUCTION

Let the space of the variable x with the distribution function F(x) be divided into r parts (classes) without common points. The corresponding values of the given probability function will be denoted by  $p_1, p_2, \ldots, p_r$  ( $\Sigma p_r = 1$ ) The test statistic  $X^2$  of the classical Chi-square test of goodness-of-fit is defined by

$$X^{2} = \sum_{i}^{r} (\mathbf{v_{i}^{2}/N \cdot p_{i}}) - N$$
 (1)

where v are the observed and N.p. = v the expected class i frequencies. For the particular case, that all the expected frequencies are equal to  $v_0 = N/r$ , equ.(1) takes the form

$$X^2 = \sum_{i=1}^{r} v_i^2 / v_o - N \tag{2}$$

It is evident that  $X^2$  is, in this case, invariant under permutations of the order of the observed frequencies v. For example, if N=8, r=2, v = 4, then  $X^2=8.0$  as well for  $v_1=0$ ,  $v_2=8$  as for  $v_1=8$ ,  $v_2=0$ .

The test statistic X<sup>2</sup>, which is a variable of the discrete type, has, in this example, the total mass of its distribution concentrated in the five mass points: 0,0.5,2.0,4.5 and 8.0. If we, alternatively, introduce a new test statistic VJ, defined by the possible pairs of observed class frequencies, which may be regarded as the coordinates of the mass points, that is

$$VJ = (v_1, v_2) \tag{3}$$

then the total mass of its distribution is concentrated in the nine points:  $(0,8),(1,7),\ldots,(8,0)$ . Thus it can be said that X is derived from VJ by a procedure which is equivalent to the pooling of classes of a continuous test statistic. It is easily proved that a pooling procedure can never increase the decision power of a test operator (Cf.Reference [1]), but may, in some cases, catastrophically reduce it, as will be illustrated in the sequel. A more general definition of VJ, than that given by equ.(3), will now be presented.

### SIGNIFICATION OF THE SYMBOL VJ

The symbol VJ will be used to denote as well a test operator as a test statistic. The test operator VJ is defined by the procedure of dividing the space of the variable x into an arbitrary number r of classes with the upper limits c<sub>1</sub>,c<sub>2</sub>,...,c<sub>r</sub> which may be selected without regard to any distribution function. Such an operator may be denoted by VJA. Alternatively, the division of the space can be specified by the class probabilities p<sub>1</sub>, in which case it may be preferable to take all the probabilities equal to

$$p_{i} = 1/r \tag{4}$$

The corresponding class limits for any hypothetical distribution function  $F(\mathbf{x})$  are then given by

$$c_i = F^{-1}(i/r) - F^{-1}((i-1)/r)$$
 (5)

If F(x) is the distribution function of the population R, the operator may be denoted by VJR. The result of its acting upon random samples from the population S may be denoted by VJRS.

From any given sample  $x_1, x_2, \dots, x_N$  the number of elements falling within the i:th class, that is, the observed frequency  $v_i$ , is determined. The value of the test statistic VJ, thus obtained, will be denoted by

$$VJ = (v_1, v_2, \dots, v_r) \quad (\Sigma v_i = N)$$
(6)

where the  ${\bf r}$  values  ${\bf v}_{\tt i}$  may be regarded as the coordinates of the mass points of  ${\bf v}_{\tt i}$  the distribution of the statistic VJ.

### III

### FUNDAMENTAL PROPERTIES OF THE STATISTIC VJ

The statistic VJ is a variable of the discrete type. The total mass of its distribution is concentrated in a finite number K of mass points, where

$$K = (N + r - 1)?/N?(r - 1)?$$
 (7)

In the particular case of pseudo-standardized samples, defined by the sample elements

$$t_{i} = (x_{i} - x_{i})/(x_{i} - x_{i})$$
 (8)

the number of non-fixed elements of the sample is reduced to (N-2), since  $t_0=0$ ;  $t_N=1$ . Thus the number of mass points becomes

$$K_{+} = (N + r - 3)!/(N - 2)!(r - 1)!$$
 (9)

Some values of K, are presented in Table 1.

These many mass points may be brought together into groups, called types of VJ. Each type consists of all possible permutations of a given set of values of v. The number of different types are listed in Table 2 for some values of N and r.

As an illustration, the types and the corresponding numbers of permutations are given for N = 10, r = 4 and r = 8, pseudo-standardized samples. in Table 3.

The number of permutations NP is given by the formula

$$NP = (N-2)!/n_1!n_2!n_3!$$
 (10)

where  $n_1$  = the number of frequencies  $v_1$ ,  $n_2$  that of frequencies  $v_2$ , and so on. Hence

$$\Sigma n_i v_i = N - 2 \tag{11}$$

Also the values of  $X^2$ , corresponding to each type of VJ are included in Table 3.

The statistical properties of VJ are completely described by its distribution, that is, the set of probability masses p of each of the K or  $K_{t}$  mass points. This distribution can be computed, for any given situation, by means of Monte-Carlo studies, as will be described in the following.

Even with modern computers the number K will be too large for large enough samples, and some kind of pooling may

be required.

From Table 3 different stages of pooling may be distinguished. The total number of mass points  $\mathbf{K}_{t}$  may be grouped according to:

- 1. The types of VJ
- 2. The values of  $X^2$
- 3. The number NE of empty classes

with a reduction of the number of mass points as indicated below for N = 10.

Stage of pooling	Nr. of ma	ass points
Stage of pooling	r = 4	r=8
VJ, ungrouped	165	6435
Types of VJ	15	22
$x^2$	14	18
NE	4	8

The reduction of the decision power due to the poolings will be illustrated below.

The test operators VJ may, just like other operators, be made to act upon three different types of samples, transformed by use of the following formulas:

1. 
$$u_i = x_i - x_1$$
 producing location invariance

2. 
$$s_i = x_i/x_N$$
 producing scale invariance (12)

3. 
$$t_i = (x_i - x_1)/(x_N - x_1)$$
 producing both scale and location invariance

If the distribution function, including its shape parameter, if any, is known, then the sample  $[u_{\cdot}]$  depends only on the scale parameter  $\beta$ , and the sample [s] only on the parameter quotient  $\mu/\beta$ . In any case, the sample  $[t_{\cdot}]$  depends only on the shape parameter  $\alpha$ .

These three types of operations may be used for two different purposes

- 1) to decide, with known decision power, between two different values of  $\beta$ ,  $\mu/\beta$ , or  $\alpha$ , and
- 2) to test whether an assumed value of these parameters is acceptable on the basis of a preassigned level of significance.

The present report will deal only with the shape operators.

### IV

### THE SHAPE PARAMETER AND ITS DECISION POWER

The most important property of an operator, its decision power DP, is determined by comparing the distributions of the actual test statistics. It is evident that these distributions depend not only on N and r but also on the class limits selected. Thus, the fundamental problem will be to determine that set of class limits which will yield the highest decision power.

To this purpose the computer programs 1/72, 2/72, and 3/72 have been written by Göran W.Weibull. A large number of random samples, usually 10,000, of a given size N and belonging to a normal population or Weibull distribution with given shape parameter  $\alpha$  are generated and transformed into t\_-samples. For an arbitrary set of class limits t\_, the frequency functions of the test statistic VJ =  $(v_1, v_2)$  (Program 1/72) VJ =  $(v_1, v_2, v_3)$  (Program 2/72) and VJ =  $(v_1, v_2, v_3, v_4)$  (Program 3/72) are determined. From the obtained frequency dbns, the decision powers have been computed for various combinations of normal and Weibull distributions and class divisions. The results for the dbns: 1.0, 0.1, 0 and N = 6,10,20, r = 2,3,4 are listed in Table 4, and N = 6,10,20; r = 4 and  $\alpha = 1.0,0.9,0.7,0.5,0.3,0.1$ , and 0 (normal dbn) in Table 5, where also the estimation powers EP (Cf.Ref[1]) are

The EP of the most powerful shape operator, so far obtained, denoted by T(i,j,k), is also presented for N=20 and is found to be somewhat lower than that of VJ.

given.

# THE USE OF VJ FOR TESTING THE ACCEPTABILITY OF AN ASSUMED DISTRIBUTION FUNCTION

Suppose, for illustration purpose, that we will test whether a given sample of size N=10 is drawn from a normal population or not by use of the shape operator VJ specified by the class limits  $t_{\rm c}=0$ , 0.250, 0.375, 0.500, 1.

After having transformed the sample into a t-sample by use of equ.(8), the number of elements v within each of the four classes are determined. This procedure yields a test point

$$VJ = (v_1, v_2, v_3, v_4) \quad (\Sigma v_i = 8)$$

The question now arises whether this test value is acceptable or not. To this purpose the distribution of VJ is computed by use of Program 3/72 which generates 10,000 random normal samples and counts the number v corresponding to each of the 165 mass points. If v the number corresponding to the actual test point is zero or very small, the hypothesis of normality will be rejected.

The critical value of  $\mathbf{v}_{\mathbf{v}}$  can be put in relation to a preassigned level of significance e by use of a statistic called the test level and denoted by TL (Cf.Ref.[1]). It is thus defined: Let n, be the number of mass points which have a  $\mathbf{v}_{\mathbf{v}}$  = i (i = 1,2,13,...), then

$$TL = \Sigma(i.n_i)/\Sigma v_v$$
 (13)

that is, TL is equal to that relative number of mass points which have v i. In this way there will be assigned a definite value of TL to each mass point. The computation of the TL-distribution is included as a part of Program 3/72.

The criterion of rejection now becomes: The hypothesis that the sample belongs to an assumed population is rejected if

TL ≤ e

Some values of TL are presented in Table 6,7 and 8,9,10

for N = 6, 10 and 20, respectively, and for various hypothetical distributions.

By use of these tables it is quite simple to decide whether an assumed distribution function is acceptable or not and also which of various dbn functions is the most probable one. Suppose we have obtained a test value

$$VJ_{test} = (0,1,2,5)$$

using the class limits indicated in Table 7, then four of the hypothetical dbns are acceptable, but the normal one is the most probable. Three of the dbns are rejected on the basis of a 5% level of significance.

A test value VJ = (0,1,6,1) motivates the rejection of all normal and Weibull distributions, which will be taken as a strong indication that the examined sample is not a simple but a composed one.

So far, the operator VJ has been specified by a set of class limits t selected without regard to the corresponding class probabilities p. This way of proceeding requires individual TL-tables for each hypothetical function.

It is, however, possible to produce a TL-table of more general applicability by selecting the class limits according to a given set of class probabilities, preferably all of them equal to  $p_i = 1/r$ . It seems plausible that we then will have the correct individual TL-functions by using the (r+1) class limits

$$t_c = F^{-1}(c/r) \quad (c = 0, 1, ..., r)$$
 (15)

This statement seems self-evident when the operator is acting upon a sample, where the non-ordered elements are independent of each other, but not at all, when it is acting upon a t-sample, where the elements within each sample form an individual entirety.

The important hypothesis that an operator VJ, defined by a given set of class probabilities (instead of a set of class limits t<sub>c</sub>), yields a distribution which can be used for any distribution function, provided that the class limits are selected according to equ.(15), has been proved by use of three different tests in the following way:

Program 3/72 was applied to 3x10,000 random t-samples of size N-2=8, drawn from the normal, the Weibull,  $\alpha=1.0$ , and the Weibull,  $\alpha=0.1$ , populations. The expected frequencies  $\mathbf{v}$  of the 3x165 mass points of VJ were determined for V the class limits V0.000, 0.500, 0.697, 1.0; V0.763, 1.0, respectively. These class limits yield class probabilities with insignificant deviations from V0.25%.

The sign test is based on the signs of the differences between the corresponding values of v. If some of the differences are zero, they will be excluded and the sample size reduced. The number of positive and negative differences are listed in the first column of the sign test. The sample size is equal to their sum. If r denotes the number of times the less frequent sign occurs, Table A-10a of Ref.[2] gives the critical value of r for 1, 5, 10, and 25 per cent levels of significance. From this table the values listed in the second column of the sign test have been taken. For example, for one plus sign and eleven minus signs, the size = 12, r = 1. A value of r less than or equal to 1 is rejected on the 1% level of significance.

Of the 28 tested samples there are

l where the sample size is too small for decision
l where the hypothesis is rejected on the 1% level
3 " " " " " " " 5% "
1 " " " " 10% "
22 " " " " " " " " " 55% "

There is no reason to reject the hypothesis on the whole.

The number-of-runs test is used for testing the random arrangement of the plus and the minus signs. The total numbers of runs observed are listed in the first column of the nr-of-runs test, and in the second column the chance of obtaining a value less than or equal to these numbers, taken from Table A -11 of Ref.[2]. On the whole, rejection of the hypothesis seems unmotivated.

The rank-sum test provides another means of testing the hypothesis. The two samples are arranged in order of size and rank scores are assigned to the individual observations. The sums of the ranks of each sample are denoted by T<sub>1</sub> and T<sub>2</sub>. Table A-20 of Ref.[2] has been used for obtaining the rejection percentages, of which there is only one small value (2.5%). This test is strongly in favour of accepting the hypothesis.

On this condition, the three sets of v, based on 30,000 random samples, can be pooled. The corresponding TL-values have been computed and are presented in Table 12, which is applicable to any hypothetical distribution, if the test value VJ have been determined by use of the class limits given by equ.(15). The limits for r=4 and r=8 are identical with the percentiles listed in Table 13.

A graphical representation of these percentiles as functions of the shape parameter  $\alpha$  of the Weibull distribution is shown in Fig.1. This graph is quite useful for a determination of the test value of VJ. Since the given sample has been transformed into a t-sample, the order statistics to may be plotted on a separate paper using the scale of the contraction of the sample elements within each of the classes are easily counted for any wanted  $\alpha$ .

It is of interest to note that the percentiles of the normal distribution, which are plotted against  $\alpha=0$ , coincide very closely with those of  $\alpha=0.28$ . Hence, there will be no possibility of deciding between these two distributions by means of the operator VJ.

### V١

# THE EFFECT OF POOLING ON THE DECISION POWER OF VJ

In the table on page 4, three different stages of pooling the probability masses of the statistic VJ and the corresponding reduction of the number of its mass points have been indicated. It is expected that these considerable reductions will strongly affect the decision power.

For illustration purpose, the shape operator VJ, pseudostandardized variables, N=10,  $t_c=0$ , 0.250, 0.375, 0.500, 1.0, will be taken as an example.

From the tables of the expected frequencies v, corresponding to the 165 mass points and computed by use of Program 3/72, the expected values of v, corresponding to each of the mass points of the reduced sets, are obtained by summing the v-values within each group. In this way the required probability distributions are easily computed, and from them the decision powers. The results are listed in Table 14, which demonstrates the catastrophic effect of the poolings on the decision powers, and, in particular, the weak decision power of the test statistic X of the Chi-square test of goodness-of-fit. This result implies that this test will, except for very large samples, frequently fail to reject false hypothetical distributions.

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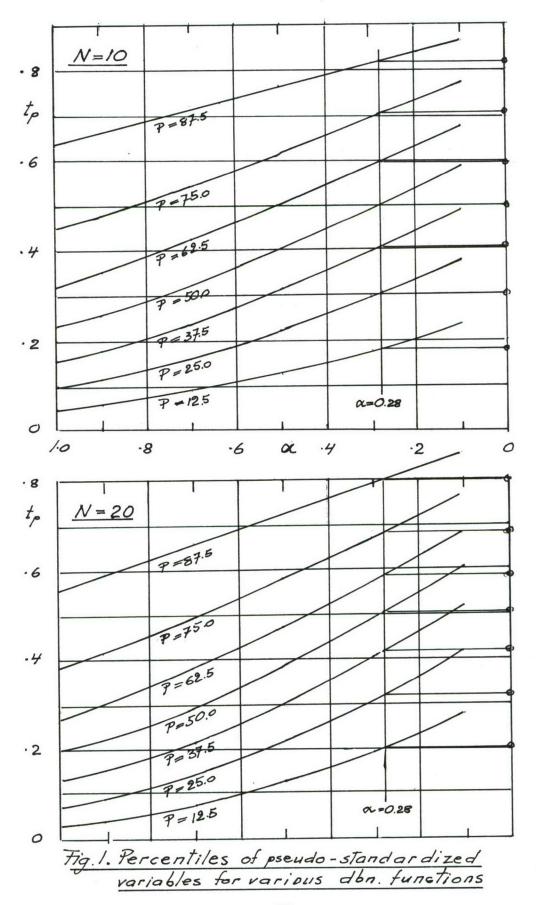


Table I. Number of mass points Kt for some N and r

N-2 r	2	3	4	5	6	7	8	
2 3 4 5 6 7 8 9 10 11 12 13 18 23 28 33 38 43	3 4 5 6 7 8 9 10 11 12 13 14 19 24 29 34 49	- 10 15 21 28 36 45 55 66 78 91 105 190 435 595 780 990 1225	- 35 56 84 120 165 220 286 364 455 560 1330 2600 4495	- 126 210 330 495 715 1001 1365 1820 2380 7315	- - 462 792 1287 2002 3003 4368 6188	- - - 1716 3003 5005 8008	6435	

Table II. Number of different types of VJ for some N and r, pseudo-standardized samples

N-2 r	2	3	4	5	6	7	8	9	10
2	2	-	-	-	-	-	_	_	_
3	2	3	-	-	-	-	_	_	_
4	3	4	5	-	-	-	_	-	_
5	3	5	6	7	_	-	_	_	_
6	4	7	9	10	11	***	_	_	_
7	4	8	11	13	14	15	_	-	_
8	5	10	15	18	20	21	22	-	-
9	5	12	18	23	26	28	29	30	-
10	6	14	22	29	34	37	39	40	41

Table III. Different types of VJ for N = 10, r = 4 and 8, pseudo-standardized samples

		r	= 4			1	c = 8				
	Type of VJ	p	r.of ermu- ions	x <sup>2</sup>		Type of VJ		of		. of ermu- tions	<b>x</b> <sup>2</sup>
1	8000	4	4	24	1	8000,0008	8	8	56		
2 3 4 5	0017 0026 0035 0044	12 12 12 12	42	17 12 9 8	2 3 4 5	0000.0017 0000.0026 0000.0035 0000.0044	56 56 56 28	196	42 32 26 24		
6 7 8 9	0116 0125 0134 0224 0233	12 24 24 12 12	84	11 7 5 4 3	6 7 8 9	0000.0116 0000.0125 0000.0134 0000.0224 0000.0233	168 336 336 168 168	1176	30 22 18 16 12		
11 12 13 14 15	1115 1124 1133 1223 2222	4 12 6 12	35	6 3 2 1 0	11 12 13 14 15	0000.1115 0000.1124 0000.1133 0000.1223 0000.2222	280 840 420 840 70	2450	20 14 12 10 8		
		tal			16 17 18 19	0001.1114 0001.1123 0001.1222 0011.1113	280 1120 560 168	1960	12 8 6		
					20	0011.1122	420	588	4 2		
					21	0111.1112	56	56	0		
					22	111101111	Total	6435			

Table IV. Decision power DP of the shape operator VJ, pseudo-standardized variables

Class limits	.125	.250	• 375	•500	.625	•750	.875
	-		72: N =				
1.0 vs 0.1	46.0	50.1				35.3	22.0
1.0 vs 0 0.1 vs 0	41.2	43.9	the same of the same of the same of		30.1	26.3	15.4
0.1 VS 0	4.9	9.1	The Real Property lies	Statement of the last of the l	11.8	9.0	6.9
1.0 vs 0.1	65.6	73.9	72: N = 74.2			50.0	34.7
1.0 vs 0	60.8	64.0	60.9	55.1	46.3	32.6	31.7
0.1 vs 0	8.2		18.0	20.6		17.5	11.6
1.0 vs 0.1	Progr 91.1	94.2	2: N = 93.9	20 ; r :		70.8	46.7
1.0 vs 0	85.2	88.4	85.0	77.8	65.0	49.3	31.5
0.1 vs 0	14.3		31.1	35.9		29.5	19.4
Class limits	.125 .250	·250	• 37 5 • 500	.500 .625	.625 .750	.750 .875	
	Progr		2: N =				1
1.0 vs 0.1 1.0 vs 0	50.1	53.6	51.8	50.5	41.9	35.3	1
1.0 vs 0 0.1 vs 0	43.9	45.5 10.8	42.8 13.1	40.0	30.1 11.8	26.3	
			2: N =				1
1.0 vs 0.1	73.9	75.6	74.5	69.9	61.2	50.0	1
1.0 vs 0 0.1 vs 0	59.8 14.9	65.4 18.0	61.2	53.1 21.5	46.3	34.0 17.5	
			2: N =			110)	1
1.0 vs 0.1	94.6	95.1	93.6	90.7	84.3	71.1	1
1.0 vs 0 0.1 vs 0	89.3	88.6		77.8 37.1	65.4 36.0	49.7 30.6	
	.125	.250	•375	.500	.625	7	J
Class limits	.250	.375	.500	.625	.750		
	• 375	.500	.625	•750	.875	4	
1.0 vs 0.1	Progra	$\frac{3}{55.2}$	$\frac{2: N = 0}{52.5}$	6; r = 6	4	_	
1.0 vs 0		45.8	52.5 42.4	50.5	30.2		
0.1 vs 0	11.3	13.1	13.5	13.2	11.8		
10 == 0.1	Progra	$\frac{2m}{3}$	2: N = ]	l0;r=	4		
1.0 vs 0.1 1.0 vs 0	77.2 68.3	69.1	74.7 62.5	70.5	61.6		
0.1 vs 0	19.6	22.0	23.0	22.7	20.9		
1001	Progra	m 3/72	2: N = 2	20 ; r =	4		
1.0 vs 0.1 1.0 vs 0	95.8		94.2 85.6	91.4			
0.1 vs 0	32.9	37.4	38.9	39.0	65.4 37.3		
					-	-	

Table V. Decision power DP of the shape operator VJ,
pseudo-standardized variables

N = 6; r = 4;  $t_0 = 0$ ; 0.250; 0.375; 0.500; 1.000

α	1.0	0.9	0.7	0.5	0.3	0.1	normal
1.0	-	6.1	18.3	31.6	44.4	55.2	45.8
0.9	6.1	-	11.1	26.0	39.7	50.7	41.1
0.7	18.3	11.1	-	14.2	29.0	41.6	30.8
0.5	31.6	26.0	14.2	-	15.6	29.1	17.6
0.3	44.4	39.7	29.0	15.6	-	15.2	3.0
0.1	55.2	50.7	41.6	29.1	15.2	-	13.1
normal	45.8	41.1	30.8	17.6	3.0	13.1	_
EP	61.0	57.3	63.2	74.5	77.0	76.0	-

N = 10; r = 4;  $t_c = 0$ ; 0.250; 0.375; 0.500; 1.000

α	1.0	0.9	0.7	0.5	0.3	0.1	normal
1.0 0.9 0.7 0.5 0.3 0.1	9.5 28.5 47.8 65.2 77.2	20.5	20.5	40.9 23.6 - 26.1	65.2 59.6 45.2 26.1 -		69.1 61.2 46.9 27.4 7.0 22.0
normal	69.1	61.2	46.9	27.4	7.0	22.0	_
EP	95.0	100.0	110.2	124.2	125.5	120.5	-

N = 20; r = 4;  $t_c = 0$ ; 0.125; 0.250; 0.375; 1.000

	-						
α	1.0	0.9	0.7	0.5	0.3	0.1	normal
1.0	-	19.8	49.3	75.9	89.8	95.8	90.7
0.9	19.8	-	37.2	67.4	85.3	93.4	86.8
0.7	49.3	37.2	-	40.5	71.6	85.2	72.1
0.5	75.9	67.4	40.5	-	41.4	68.0	46.2
0.3	89.8	85.3	71.6	41.4	-	38.1	13.9
0.1	95.8	93.4	85.2	68.0	38.1	-	32.9
normal	90.7	86.8	72.1	46.2	13.9	32.9	-
EP :	198.0	190.0	194.2	204.8	198.8	190.5	_

EP(T) 173.7 175.9 188.3 202.2 198.7 188.7

Table VI. Test levels of the mass points VJ, pseudo-standard. variables, N = 6,  $t_c = 0$ , 0.250, 0.375, 0.500, 1.000

Mass	points		Hypot	hetica	l dist	ributi	ons	
No.	VJ	$\alpha = 1.0$	0.9	0.7	0.5	0.3	0.1	normal
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35	0004 0013 0022 0031 0040 0103 0112 0121 0130 0202 0211 0220 0301 0310 0400 1003 1012 1021 1030 1102 1111 1120 1201 1210 1300 2002 2011 2020 2101 2110 2200 301 3010 3100 400	4.0 9.4 4.0 0.9 0.0 8.2 12.4 2.6 0.1 4.9 5.8 0.5 1.3 0.0 25.7 35.1 16.0 0.7 45.5 40.2 7.0 22.3 10.8 2.6 73.0 58.1 190.3 35.1 190.3 190.3	5.8 9.8 3.0 1.1 0.0 11.3 16.2 3.9 0.2 7.0 5.8 0.8 1.5 0.6 0.1 29.1 42.8 18.3 0.4 60.6 53.9 25.0 12.8 21.8 67.3 14.4 100.0 37.8 21.6 100.0 33.2 74.0	13.2 25.4 8.2 1.2 0.1 22.7 31.0 8.2 0.3 15.0 0.1 50.8 63.5 28.2 0.5 0.7 37.4 13.2 2.8 84.2 76.7 5.4 100.0 41.3 20.0 70.0 33.8 45.4	34.2 42.3 19.4 3.2 0.1 46.9 51.6 15.2 0.4 21.8 9.8 1.0 2.5 7 0.2 83.8 91.8 27.4 100.0 63.3 8.2 30.7 6.8 1.5 55.5 56.5 24.5 11.6 37.9 13.3 17.2	74.3 82.0 27.1 3.3 0.2 59.4 52.3 13.5 0.6 23.5 11.6 0.3 0.1 100.0 90.7 20.8 1.6 74.3 40.6 8.4 18.1 7.4 0.9 46.4 35.4 5.7 31.2 10.0 4.9 10.0 4.9 10.0 4.9 10.0 4.9 10.0 4.9 10.0 4.9 10.0 4.9 10.0 4.9 10.0 4.9 10.0 4.9 10.0 4.9 10.0 4.9 10.0 4.9 10.0 4.9 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10	100.0 84.9 24.1 4.3 0.1 62.2 38.5 9.4 0.4 15.3 7.0 1.0 2 0.2 0.0 73.2 53.3 13.0 0.3 45.4 28.1 3.8 11.0 2.8 0.6 32.9 17.8 2.0 20.5 5.2 2.0 3.0 2.0 3.0 2.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3	51.0 13.0 0.6 22.8 11.0 1.2 2.3 0.0 100.0 73.6 19.9 1.5 65.4 39.4 6.1 17.3 8.0 1.2 45.0 34.3 3.0 26.3 9.4 4.4

Table VIL Test levels of the mass points VJ, pseudo-standard. variables, N = 10,  $t_c = 0$ , 0.250, 0.375, 0.500, 1.000

Mass	points		Hypot	heti <b>c</b> a	l dist	ributi	ons	
No.	VJ	$\alpha = 1.0$	0.9	0.7	0.5	0.3	0.1	normal
1 2 3 4 5 6 7 8 9 0 11 12 13 14 15 16 17 18 19 20 12 22 23 24 25 26 27 28 29 30 31 33 33 34 35 36 37 38 38 38 39 39 39 39 39 39 39 39 39 39 39 39 39	0008 0017 0026 0035 0044 0053 0062 0071 0080 0107 0116 0125 0134 0143 0152 0161 0170 0206 0215 0224 0233 0242 0251 0260 0305 0314 0323 0341 0350 0404 0413 0422 0431 0440 0503 0512 0521 0530 0602 0611 0620	0.1 0.1 0.0 0.2 0.0 0.0 0.0 0.0 0.0 0.0	0.1 0.6 0.5 0.3 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.5 1.2 0.9 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	3.6 10.8 7.6 5.5 1.6 0.8 0.0 0.0 9.8 26.3 15.7 2.8 0.1 0.9 1.8 26.3 10.8 0.5 0.6 28.8 26.3 10.8 0.6 0.6 28.8 26.3 10.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	19.9 57.9 47.8 19.0 6.6 1.1 0.0 0.0 38.9 7.5 0.4 0.1 0.0 30.4 56.1 33.8 11.2 2.7 0.0 16.0 0.1 0.0 16.0 17.0 16.0 17.0	94.0 100.0 57.9 28.1 7.3 1.4 0.0 0.0 67.8 79.6 49.0 19.4 6.3 0.0 0.0 37.9 39.9 25.4 8.9 1.6 0.1 0.0 11.4 12.6 6.3 2.2 0.0 1.5 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6	35.6 73.2 59.4 24.6 10.1 2.9 0.0 50.3 92.5 86.3 25.5 8.2 0.0 37.0 933.2 15.4 6.3 0.0 14.9 18.8 13.8 6.3 0.0 14.9 18.8 13.8 6.3 0.0 14.9 15.0 16.

TableVII (Continued)

Mass	points		Hypot	heti <b>c</b> a	l dist	ributi	ons	
No.	VJ	$\alpha = 1.0$	0.9	0.7	0.5	0.3	0.1	normal
43	0701	0.0	0.0	0.0	0.0	0.0	0.0	0.0
44	0710	0.0	0.0	0.0	0.0	0.0	0.0	0.0
45	0800	0.0	0.0	0.0	0.0	0.0	0.0	0.0
46	1007	0.9	1.4	6.4	19.2	46.2	75.1	38.4
47	1016	1.9	2.7	9.2	44.2	86.3	84.4	83.5
48	1025	2.6	4.6	10.8	40.6	73.1	61.0	68.3
49	1034	1.6	2.7	8.5	19.8	37.6	26.7	30.8
50	1043	0.9	0.8	1.8	6.1	14.8	6.3	10.9
51	1052	0.0	0.1	0.3	1.5	1.8	1.2	1.8
52	1061	0.0	0.0	0.1	0.1	0.8	0.0	0.7
53	1070	0.0	0.0	0.0	0.0	0.0	0.0	0.0
54	1106	1.1	3.6	9.2	32.4	68.4	71.4	75.7
55	1115	7.2	10.4	40.1		100.0		100.0
56	1124	7.5	9.4	30.4	77.2	92.4	64.1	89.4
57	1133	3.2	6.6	15.9	44.2	40.3	17.4	48.7
58	1142	0.2	1.4	3.1	15.7	8.9	7.0	12.8
59	1151	0.0	0.0	0.6	0.5	0.8	0.4	0.8
60	1160	0.0	0.0	0.0	0.0	0.0	0.0	0.0
61	1205	3.8	5.1	12.9	37.4		34.2	47.1
62	1214	7.9	14.2	41.3	74.9		42.0	80.8
63	1223	6.1	7.4	28.5	65.0		22.8	55.3
64	1232	1.9	4.6	16.5	21.8	20.7	8.5	18.1
65	1241	0.9	0.5	1.8	3.6	3.8	2.7	4.3
66	1250	0.0	0.0	0.0	0.3	0.1	0.0	0.0
67	1304	3.2	4.2	15.4	23.3	23.3	13.8	21.2
68	1313	6.5	7.8	25.8	55.5	29.4	16.5	34.4
69	1322	3.4	4.2	13.4	33.3	16.6	5.4	16.6
70	1331	0.5	1.7	5.4	5.5	5.4	1.2	4.8
71	1340	0.0	0.0	0.2	0.2	0.2	0.0	0.5
72	1403	2.6	3.4	4.7	7.6	4.5	2.4	0.3
73	1412	1.4	3.8	8.5	15.7	7.5	3.9	6.8
74	1421	1.1	1.4	4.2	4.7	2.5	1.2	2.3
75	1430	0.4	0.5	0.5	0.5	0.1	0.2	0.5
76	1502	1.2	0.6	1.2	1.5	1.1	0.5	0.7
77	1511	0.4	1.4	2.6	1.9	0.8	0.2	0.7
78	1520	0.0	0.0	0.3	0.1	0.0	0.1	0.3
79	1601	0.1	0.3	0.2	0.2	1.1	0.0	0.3
80	1610	0.0	0.1	0.1	0.2		0.0	0.5
81	1700	0.0	0.0	0.0	0.0	0.0	0.0	0.0

TableVII (Continued)

Mass	points		Hypot	hetica	l dist	ributi	ons	
No.	VJ	$\alpha = 1.0$	0.9	0.7	0.5	0.3	0.1	normal
82	2006	3.2	3.4	7.4	24.0	44.7	44.1	45.6
83	2015	7.2	11.4	37.7	72.8	89.2	52.0	66.0
84	2024	9.6	13.1	33.5	63.4		37.9	57.3
85	2033	4.1	6.3	17.1	30.6		15.1	22.8
86	2042	0.9	2.1	6.4	12.8	5.2	3.4	5.5
87	2051	0.1	0.5	0.9	1.2	0.4	0.5	0.3
88	2060	0.0	0.0	0.0	0.0	0.1	0.0	0.0
89	2105	13.9	22.4	51.0	70.8	70.7	46.4	61.4
90	2114	20.6	36.7	87.3	100.0	95.9	54.9	96.1
91	2123	21.7	31.5	75.5	89.7	80.8	32.5	78.2
92	2132	13.2	15.5	33.5	55.5		12.6	24.6
93	2141	2.3	1.7	6.4	8.5	4.1	1.2	5.2
94	2150	0.0	0.5	0.3	0.1	0.1	0.0	1.2
95	2204	12.6	18.6	45.2	51.1	54.3	21.6	53.6
96	2213	25.0	47.1	89.8	92.8	68.4	29.5	70.7
97	2222	16.1	25.5	67.2	68.8	41.8	14.4	41.2
98	2231	4.6	9.9	14.3	16.8	12.7	4.7	8.9
99	2240	0.4	0.3	0.9	1.2	0.2	0.0	1.2
100	2303	10.5	17.0	29.5	34.3	17.4	6.6	20.4
101	2312	15.3	23.4	49.5	51.1	26.3	8.1	22.0
102	2321	10.0	12.0	21.1	19.2	8.5	1.8	9.3
103	2330	2.0	1.5	2.3	4.0	0.8	0.1	1.2
104	2402	5.5	8.6	11.6	15.7	3.6	1.2	3.6
105	2411	4.9	7.4	10.8	13.3	6.6	1.2	3.9
106	2420	1.6	1.4	2.3	1.2	1.4	0.1	1.2
107	2501	2.2	2.1	1.5	1.9	1.1	0.2	0.7
108	2510	0.5	0.6	1.5	0.5	0.0	0.0	0.3
109	2600	0.1	0.1	0.3	0.1	0.0	0.0	0.0
110 •	300)	12.1	14.8	23.4	36.3	29.4	18.3	29.6
111	3014	23.8	30.2	54.2	66.8	50.9	31.0	44.1
112	3023	18.7	27.8	49.5	63.4	35.0	13.8	32.0
113	3032	10.9	13.1	19.0	24.8	14.8	5.4	10.5
114	3041	1.4	2.1	6.4	4.0	2.5	0.2	1.8
115	3050	0.0	0.1	0.6	0.0	0.8	0.0	0.1
116	3104	31.8	45.5	61.3	63.4	49.4	20.4	42.7
117	3113	62.1		100.0	96.3	75.6	24.0	63.6
118	3122	46.7	68.8	82.4	86.8	43.2	15.1	39.8
119	3131	11.5	17.0	24.2	20.5	10.2	3.5	8.9
120	3140	0.4	2.3	1.8	1.9	0.4	0.5	1.2
121	3203	37.8	52.2	71.2	48.2	27.3	11.4	26.4
122	3212	69.8	82.8	96.6	81.9	36.3	10.3	28.5
123	3221	30.4	40.9	57.7	45.5	9.8	3.4	16.0
124	3230	3.2	4.8	12.9	8.5	3.6	0.8	2.0

Table VII (Continued)

Mass	points		Hypot	hetica	l dist	ributio	ns	
No.	VJ	$\alpha = 1.0$	0.9	0.7	0.5	0.3	0.1	normal
125	3302	27.6	39.5	43.8	35.3	12.2	2.2	14.3
126	3311	26.2	34.1	59.5	39.5	8.5	2.4	7.5
127	3320	4.3	6.C	8.5	5.5	1.1	0.6	2.1
128	3401	8.3	10.9	10.0	8.5	3.6	0.6	1.8
129	3410	3.8	3.0	5.1	3.6	1.4	0.1	2.0
130	3500	0.9	1.0	2.0	0.3	0.2	0.1	0.0
131	4004	19.6	21.4	26.6	28.8	15.4	8.1	12.3
132	4013	41.1	56.0	63.2	58.5	18.2	9.8	17.4
133	4022	39.4	26.6	46.6	38.4	10.7	4.9	11.8
134	4031	8.7	8.6	14.3	9.8	3.6	0.4	1.8
135	4040	0.9	2.3	0.5	0.3	0.8	0.2	0.0
136	4103	59.6	71.2	69.2	57.0	22.5	9.3	19.6
137	4112	91.7	100.0	93.2	79.5	31.5	7.3	27.4
138	4121	48.6	62.1	73.3	41.8	9.3	4.7	13.8
139	<b>41</b> 30	9.6	9.0	6.8	4.5	1.4	0.0	1.8
140	4202	75.4	79.7	77.7	46.8	13.2	3.9	11.8
141	4211	81.4	89.2	84.8	55.5	13.7	1.4	9.7
142	4220	17.8	17.8	19.0	12.8	2.5	0.5	3.2
143	4301	34.7	45.5	36.6	21.2	2.5	0.7	3.9
144	4310	14.6	19.6	25.8	6.6	1.8	0.2	1.2
145	4400	6.1	5.6	2.6	2.8	0.4	0.1	0.5
146	5003	33.2	38.1	31.4	18.0	6.8	2.2	5.2
147	5012	67.2	66.5	52.6	22.6	5.0	1.5	6.6
148	5021	36.3	29.0	21.8	11.6	4.5	1.2	2.7
149	5030	5.2	5.4	4.7	1.5	0.8	0.2	0.8
150	5102	87.9	92.4	67.2	30.6	6.6	1.8	4.5
151	5111	100.0	96.1	80.0	31.4	8.5	1.4	8.2
152	5120	30.4	34.1	22.6	9.1	2.8	0.0	1.3 4.3
153	5201	84.5	76.7	55.9	17.4	3.6 1.6	0.5	2.3
154	5210	50.7	54.0	38.9 14.8	15.7 3.0	0.8	0.0	0.3
155	5300	22.7	20.5		7.6	1.9	0.8	2.7
156	6002	52.8	58.0	27.5	6.1	1.5	0.1	2.9
157	6011 6020	64.6	13.6	34.5 12.0	3.6	0.1	0.0	0.1
158		16.9						1.4
159	6101	95.8		35.6	10.1	1.4	0.2	0.7
160	<b>61</b> 10 6200	72.6	64.3 48.8	21.1	4.2	0.8	0.1	0.1
161 162	7001	57.3	42.4	19.0	2.1	0.4	0.1	0.5
163	7010	44.8	36.7	11.6	0.8	0.1	0.1	0.0
164	7100	78.3	60.0	19.6	1.5	0.2	0.0	0.3
165	8000	43.0	24,4	7.4	0.8	0.0	0.0	0.1

Table IIX. Test levels of the mass points VJ, pseudo-standardized Weibull samples,  $\alpha = 1.0$ , N = 20,  $t_c = 0$ , .125,.250,.375,1.0 Mass points not appearing in this table have a TL $\leq 1.4\%$ 

v1         v2         3         4         5         6         7         8         9           0         4         -         -         -         -         2.8         - <th></th>											
O	$\mathbf{v}_1 \mathbf{v}_2$	0	1	2	3	4	5	6	7	8	9
0   5   -	0 4	-	_	-	-	_	2.8	_	_	_	_
1 2       -       -       -       2.8       2.8       2.8       -	0 5	-	_	_	_	2.8		_	_		
1 2       -       -       -       2.8       2.8       2.8       -	0 6	_	_	2.8			-	-	-	-	
1 3 4       -       -       2.8       6.2       6.2       4.2       4.2       -	1 2	_	_	_	2.8		2.8	_	_	_	
1 4       -       -       4.2       2.8       2.8       6.2       - <td< th=""><th>1 3</th><th>_</th><th>-</th><th>2.8</th><th></th><th></th><th></th><th>4.2</th><th>_</th><th>_</th><th></th></td<>	1 3	_	-	2.8				4.2	_	_	
1 5       -       -       6.2       2.8       6.2       -		_	_					_	_	_	
1 6       -       -       -       6.2       2.8       4.2       2.8       - <td< th=""><th>1 5</th><th>_</th><th>_</th><th>6.2</th><th></th><th></th><th></th><th>_</th><th>_</th><th>_</th><th></th></td<>	1 5	_	_	6.2				_	_	_	
1 7       -       -       -       4.2       - <th>1 6</th> <th>_</th> <th>_</th> <th></th> <th></th> <th>2.8</th> <th></th> <th>2.8</th> <th>_</th> <th>_</th> <th></th>	1 6	_	_			2.8		2.8	_	_	
1       8       -	1 7	_	_	_		4.2		-	-	_	
2	1 8	-	-	-	2.8		_	_	_	_	
2 11       -       -       2.8       - <th>2 1</th> <th>_</th> <th>-</th> <th>_</th> <th></th> <th>_</th> <th></th> <th></th> <th>_</th> <th>_</th> <th></th>	2 1	_	-	_		_			_	_	
2 11       -       -       2.8       - <th>2 2</th> <th></th> <th>_</th> <th>4.2</th> <th></th> <th></th> <th>6.2</th> <th></th> <th>_</th> <th>_</th> <th></th>	2 2		_	4.2			6.2		_	_	
2 11       -       -       2.8       - <th>2 3</th> <th>_</th> <th>8.1</th> <th></th> <th></th> <th></th> <th>21.5</th> <th></th> <th></th> <th></th> <th></th>	2 3	_	8.1				21.5				
2 11       -       -       2.8       - <th>2 4</th> <th>-</th> <th>-</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>_</th> <th></th>	2 4	-	-							_	
2 11       -       -       2.8       - <th>2 5</th> <th>-</th> <th>9.9</th> <th>2.8</th> <th>28.7</th> <th></th> <th></th> <th></th> <th></th> <th>_</th> <th></th>	2 5	-	9.9	2.8	28.7					_	
2 11       -       -       2.8       - <th>2 6</th> <th>2.8</th> <th></th> <th></th> <th>8.1</th> <th></th> <th>2.8</th> <th></th> <th></th> <th>_</th> <th></th>	2 6	2.8			8.1		2.8			_	
2 11       -       -       2.8       - <th>2 7</th> <th>-</th> <th></th> <th>12.4</th> <th></th> <th>12.4</th> <th></th> <th></th> <th>_</th> <th></th> <th></th>	2 7	-		12.4		12.4			_		
2 11       -       -       2.8       - <th>2 8</th> <th>-</th> <th>-</th> <th>6.2</th> <th></th> <th>-</th> <th>4.2</th> <th></th> <th>_</th> <th>-</th> <th>-</th>	2 8	-	-	6.2		-	4.2		_	-	-
4 2       -       6.2       31.0       29.6       31.0       21.5       9.9       4.2       2.8       4.2         4 3       11.2       14.7       38.8       65.0       53.6       41.5       28.7       9.9       2.8       -         4 4       9.9       27.4       55.2       62.3       65.0       43.0       25.6       2.8       -       -         4 5       6.2       34.6       73.5       69.4       60.5       25.6       21.5       2.8       -       -         4 6       4.2       44.5       53.6       53.6       39.6       18.8       6.2       -       -       -       -         4 7       4.2       18.8       55.2       27.4       23.2       -       -       -       -       -       -         4 8       6.2       12.4       24.0       14.7       13.7       -       -       -       -       -         4 9       2.8       6.2       9.9       8.1       2.8       -       -       -       -       -       -	2 11	-	-	2.8				-	-	_	
4 2       -       6.2       31.0       29.6       31.0       21.5       9.9       4.2       2.8       4.2         4 3       11.2       14.7       38.8       65.0       53.6       41.5       28.7       9.9       2.8       -         4 4       9.9       27.4       55.2       62.3       65.0       43.0       25.6       2.8       -       -         4 5       6.2       34.6       73.5       69.4       60.5       25.6       21.5       2.8       -       -         4 6       4.2       44.5       53.6       53.6       39.6       18.8       6.2       -       -       -       -         4 7       4.2       18.8       55.2       27.4       23.2       -       -       -       -       -       -         4 8       6.2       12.4       24.0       14.7       13.7       -       -       -       -       -         4 9       2.8       6.2       9.9       8.1       2.8       -       -       -       -       -       -	3 0	-	-		-	2.8	_	_	_	_	
4 2       -       6.2       31.0       29.6       31.0       21.5       9.9       4.2       2.8       4.2         4 3       11.2       14.7       38.8       65.0       53.6       41.5       28.7       9.9       2.8       -         4 4       9.9       27.4       55.2       62.3       65.0       43.0       25.6       2.8       -       -         4 5       6.2       34.6       73.5       69.4       60.5       25.6       21.5       2.8       -       -         4 6       4.2       44.5       53.6       53.6       39.6       18.8       6.2       -       -       -       -         4 7       4.2       18.8       55.2       27.4       23.2       -       -       -       -       -       -         4 8       6.2       12.4       24.0       14.7       13.7       -       -       -       -       -         4 9       2.8       6.2       9.9       8.1       2.8       -       -       -       -       -       -	3 1	-	-	-	_	6.2		6.2	4.2		
4 2       -       6.2       31.0       29.6       31.0       21.5       9.9       4.2       2.8       4.2         4 3       11.2       14.7       38.8       65.0       53.6       41.5       28.7       9.9       2.8       -         4 4       9.9       27.4       55.2       62.3       65.0       43.0       25.6       2.8       -       -         4 5       6.2       34.6       73.5       69.4       60.5       25.6       21.5       2.8       -       -         4 6       4.2       44.5       53.6       53.6       39.6       18.8       6.2       -       -       -       -         4 7       4.2       18.8       55.2       27.4       23.2       -       -       -       -       -       -         4 8       6.2       12.4       24.0       14.7       13.7       -       -       -       -       -         4 9       2.8       6.2       9.9       8.1       2.8       -       -       -       -       -       -	3 2	-	4.2	11.2	9.9	21.5	17.1	9.9		_	-
4 2       -       6.2       31.0       29.6       31.0       21.5       9.9       4.2       2.8       4.2         4 3       11.2       14.7       38.8       65.0       53.6       41.5       28.7       9.9       2.8       -         4 4       9.9       27.4       55.2       62.3       65.0       43.0       25.6       2.8       -       -         4 5       6.2       34.6       73.5       69.4       60.5       25.6       21.5       2.8       -       -         4 6       4.2       44.5       53.6       53.6       39.6       18.8       6.2       -       -       -       -         4 7       4.2       18.8       55.2       27.4       23.2       -       -       -       -       -       -         4 8       6.2       12.4       24.0       14.7       13.7       -       -       -       -       -         4 9       2.8       6.2       9.9       8.1       2.8       -       -       -       -       -       -	3 3	2.8	12.4	23.2		27.4	37.7			-	
4 2       -       6.2       31.0       29.6       31.0       21.5       9.9       4.2       2.8       4.2         4 3       11.2       14.7       38.8       65.0       53.6       41.5       28.7       9.9       2.8       -         4 4       9.9       27.4       55.2       62.3       65.0       43.0       25.6       2.8       -       -         4 5       6.2       34.6       73.5       69.4       60.5       25.6       21.5       2.8       -       -         4 6       4.2       44.5       53.6       53.6       39.6       18.8       6.2       -       -       -       -         4 7       4.2       18.8       55.2       27.4       23.2       -       -       -       -       -       -         4 8       6.2       12.4       24.0       14.7       13.7       -       -       -       -       -         4 9       2.8       6.2       9.9       8.1       2.8       -       -       -       -       -       -	3 4	2.8	17.1		49.8					-	- 1
4 2       -       6.2       31.0       29.6       31.0       21.5       9.9       4.2       2.8       4.2         4 3       11.2       14.7       38.8       65.0       53.6       41.5       28.7       9.9       2.8       -         4 4       9.9       27.4       55.2       62.3       65.0       43.0       25.6       2.8       -       -         4 5       6.2       34.6       73.5       69.4       60.5       25.6       21.5       2.8       -       -         4 6       4.2       44.5       53.6       53.6       39.6       18.8       6.2       -       -       -       -         4 7       4.2       18.8       55.2       27.4       23.2       -       -       -       -       -       -         4 8       6.2       12.4       24.0       14.7       13.7       -       -       -       -       -         4 9       2.8       6.2       9.9       8.1       2.8       -       -       -       -       -       -	3 5		21.5		75.2		28.7			-	
4 2       -       6.2       31.0       29.6       31.0       21.5       9.9       4.2       2.8       4.2         4 3       11.2       14.7       38.8       65.0       53.6       41.5       28.7       9.9       2.8       -         4 4       9.9       27.4       55.2       62.3       65.0       43.0       25.6       2.8       -       -         4 5       6.2       34.6       73.5       69.4       60.5       25.6       21.5       2.8       -       -         4 6       4.2       44.5       53.6       53.6       39.6       18.8       6.2       -       -       -       -         4 7       4.2       18.8       55.2       27.4       23.2       -       -       -       -       -       -         4 8       6.2       12.4       24.0       14.7       13.7       -       -       -       -       -         4 9       2.8       6.2       9.9       8.1       2.8       -       -       -       -       -       -	3 6			28.7	36.7					-	-
4 2       -       6.2       31.0       29.6       31.0       21.5       9.9       4.2       2.8       4.2         4 3       11.2       14.7       38.8       65.0       53.6       41.5       28.7       9.9       2.8       -         4 4       9.9       27.4       55.2       62.3       65.0       43.0       25.6       2.8       -       -         4 5       6.2       34.6       73.5       69.4       60.5       25.6       21.5       2.8       -       -         4 6       4.2       44.5       53.6       53.6       39.6       18.8       6.2       -       -       -       -         4 7       4.2       18.8       55.2       27.4       23.2       -       -       -       -       -       -         4 8       6.2       12.4       24.0       14.7       13.7       -       -       -       -       -         4 9       2.8       6.2       9.9       8.1       2.8       -       -       -       -       -       -	3 7	4.2	11.2	18.8	32.3	13.7	6.2		-	_	-
4 2       -       6.2       31.0       29.6       31.0       21.5       9.9       4.2       2.8       4.2         4 3       11.2       14.7       38.8       65.0       53.6       41.5       28.7       9.9       2.8       -         4 4       9.9       27.4       55.2       62.3       65.0       43.0       25.6       2.8       -       -         4 5       6.2       34.6       73.5       69.4       60.5       25.6       21.5       2.8       -       -         4 6       4.2       44.5       53.6       53.6       39.6       18.8       6.2       -       -       -       -         4 7       4.2       18.8       55.2       27.4       23.2       -       -       -       -       -       -         4 8       6.2       12.4       24.0       14.7       13.7       -       -       -       -       -         4 9       2.8       6.2       9.9       8.1       2.8       -       -       -       -       -       -	3 8			21.5	18.8		-	-	-	-	
4 2       -       6.2       31.0       29.6       31.0       21.5       9.9       4.2       2.8       4.2         4 3       11.2       14.7       38.8       65.0       53.6       41.5       28.7       9.9       2.8       -         4 4       9.9       27.4       55.2       62.3       65.0       43.0       25.6       2.8       -       -         4 5       6.2       34.6       73.5       69.4       60.5       25.6       21.5       2.8       -       -         4 6       4.2       44.5       53.6       53.6       39.6       18.8       6.2       -       -       -       -         4 7       4.2       18.8       55.2       27.4       23.2       -       -       -       -       -       -         4 8       6.2       12.4       24.0       14.7       13.7       -       -       -       -       -         4 9       2.8       6.2       9.9       8.1       2.8       -       -       -       -       -       -	3 9	4.2	4.2	6.2			-	-	-	-	
4 2       -       6.2       31.0       29.6       31.0       21.5       9.9       4.2       2.8       4.2         4 3       11.2       14.7       38.8       65.0       53.6       41.5       28.7       9.9       2.8       -         4 4       9.9       27.4       55.2       62.3       65.0       43.0       25.6       2.8       -       -         4 5       6.2       34.6       73.5       69.4       60.5       25.6       21.5       2.8       -       -         4 6       4.2       44.5       53.6       53.6       39.6       18.8       6.2       -       -       -       -         4 7       4.2       18.8       55.2       27.4       23.2       -       -       -       -       -       -         4 8       6.2       12.4       24.0       14.7       13.7       -       -       -       -       -         4 9       2.8       6.2       9.9       8.1       2.8       -       -       -       -       -       -	4 1	-		6.2	21.5	8.1	12.4	6.2	2.8	-	-
4 5       6.2 34.6 73.5 69.4 60.5 25.6 21.5 2.8         4 6       4.2 44.5 53.6 53.6 39.6 18.8 6.2         4 7       4.2 18.8 55.2 27.4 23.2         4 8       6.2 12.4 24.0 14.7 13.7         4 9       2.8 6.2 9.9 8.1 2.8	4 2	-		31.0	29.6	31.0	21.5		4.2	2.8	4.2
4 5       6.2 34.6 73.5 69.4 60.5 25.6 21.5 2.8         4 6       4.2 44.5 53.6 53.6 39.6 18.8 6.2         4 7       4.2 18.8 55.2 27.4 23.2         4 8       6.2 12.4 24.0 14.7 13.7         4 9       2.8 6.2 9.9 8.1 2.8	4 3	11.2	14.7	38.8	65.0	53.6	41.5	28.7		2.8	
4 5       6.2 34.6 73.5 69.4 60.5 25.6 21.5 2.8         4 6       4.2 44.5 53.6 53.6 39.6 18.8 6.2         4 7       4.2 18.8 55.2 27.4 23.2         4 8       6.2 12.4 24.0 14.7 13.7         4 9       2.8 6.2 9.9 8.1 2.8	4 4	9.9	27.4	55.2			43.0	25.6			
4 7       4.2 18.8 55.2 27.4 23.2         4 8       6.2 12.4 24.0 14.7 13.7         4 9       2.8 6.2 9.9 8.1 2.8	4 5				69.4	60.5				_	_
4 7       4.2 18.8 55.2 27.4 23.2         4 8       6.2 12.4 24.0 14.7 13.7         4 9       2.8 6.2 9.9 8.1 2.8	4 6	4.2	44.5	53.6			18.8			-	
4 8     6.2 12.4 24.0 14.7 13.7       4 9     2.8 6.2 9.9 8.1 2.8	4 7	4.2	18.8					-	-	_	- 1
4 9   2.8 6.2 9.9 8.1 2.8	4 8	6.2	12.4				-	-	-	-	1
	4 9	2.8	6.2	9.9			-	-	-	_	-
	4 10			4.2			_	-	_	_	-

Table IIX (Continued)

$v_1$ $v_2$	0	1	2	3	4	5	6	7	8
5 0	-	-	-	4.2	2.8	4.2	2.8	-	-
5 5 5 5 5 5 5 5 5 5 6 7 8 9 0 0	-	4.2	9.9	27.4	18.8	17.1	8.1	6.2	-
5 2	-	18.8	41.5	45.7	44.5	41.5	14.7	2.8	-
5 3	6.2	31.0	65.0	80.3	77.9	57.2	17.1	6.2	-
5 4	17.1	46.4	84.9	91.7	84.9	47.7	24.0	6.2	-
5 5	27.4	63.2	76.8	93.3	71.5	32.3	17.1	-	-
5 6	21.5	39.6	73.5	49.8	36.7	18.8	6.2	-	-
5 7	4.2	34.6	47.7	44.5	21.5	6.2	-	-	-
5 8	9.9	23.2	21.5	13.7	6.2	-	-	-	-
5 9	4.2	4.2	8.1	6.2	-	-	-	-	-
5 10	-	2.8	-	-	-	-	-	_	-
	-	-	4.2	2.8	-	-	-	-	_
6 1	-	4.2	23.2	33.2	17.1	27.4	4.2	4.2	-
6 2	6.2	28.7	51.3	53.6	60.5	33.2	21.5	8.1	-
6 3	8.1	46.4	75.2	90.9	79.1	51.3	13.7	4.2	-
6 4	11.2	62.3	96.1	96.1	85.6	37.7	12.4	2.8	-
6 5	21.5	73.5	92.5	87.8	71.5	32.3	4.2	-	-
6 6	12.4	71.5	87.8	76.8	43.0	8.1	-	_	-
6 7 6 8	21.5	39.6	62.3	43.0	21.5	_	-	_	-
6 9	8.1	11.2	34.6	11.2	9.9	_	_	_	_
6 10	_	2.8	9.9	_	_	_	_		_
7 0	_	_	_	2.8	8.1	_	2.8	_	_
7 1	6.2	8.1	12.4	31.0	25.6	25.6	9.9	_	2.8
7 2	6.2	17.1	58.4	66.9	49.8	41.5	17.1	2.8	_
7 3	13.7	53.6	89.4	90.9	58.4	46.7	14.7	_	_
7 4	31.0	69.4	96.1	100.0	76.8	45.7	8.1	_	_
7 5	27.4	67.4	99.0	99.0	60.5	8.1	2.8	-	-
7 6	36.7	59.2	71.5	71.5	27.4	11.2	-	_	_
7 7	21.5	41.5	44.5	23.2	2.8	_		_	-
7 8	9.9	18.8	13.7	8.1	_	_	_		_
7 9	6.2	6.2	4.2	-	-	_	-	-	-
8 0	-	-	-	6.2	2.8	-	-	-	-
8 1	-	14.7	32.3	17.1	23.2	17.1	6.2	-	-
8 2	8.1	29.6	51.3	53.6	37.7	25.6	8.1	-	-
8 3	9.9	62.3	77.9	83.6	80.3	34.6	17.1	-	-
8 4	21.5	66.0	97.0	89.4	51.3	24.0	-	-	-
8 5 8 6	17.1	73.5	82.9	74.1	36.7	2.8	-	-	-
8 6	17.1	57.2	66.9	36.7	6.2	-	-	-	-
8 7 8 8	8.1	36.7	29.6	12.4	-	-	-	-	-
8 8	6.2	14.7	-	-	-	-	-	-	-
8 9	4.2	-	-	-	-	-	-	-	-
9 0 9 1	_	-	2.8	4.2	4.2	-	-	-	-
9 1	-	13.7	24.0	34.6	25.6	11.2	-	-	-
9 2	4.2	28.7	57.2	59.2	31.0	17.1	2.8	-	-

Table IIX (Continued)

$v_1$ $v_2$	0	1	2	3	4	5	6
9 3 4 5 6 7 8 0 1 2 3 4 5 6 7 0 1 2 3 4 5 6 0 1 2 3 4 5 1 2 1 2 1 2 1 2 1 2 1 2 1 3 1 3 1 3 1 3	18.8 27.4 23.2 17.1 18.8 4.2 9.9 8.1 17.1 29.6 14.7 11.2 6.2 21.5 13.7 21.5 6.2 2.8 2.8 2.8 2.8 3.9 2.8 3.1 12.4 4.2 9.9 6.2 2.8 3.1 12.4 4.2 9.9 6.2 2.8 3.1 4.2 9.9 6.2 2.8 8.1 12.4 8.1 4.2 9.9 6.2 2.8 8.1 12.4 8.1 4.2 9.9 6.2 2.8 8.1 12.4 8.1 12.4 8.1 12.4 8.1 8.1 8.1 8.1 8.1 8.1 8.1 8.1	66.0 69.4 55.2 43.0 25.6 8.1 27.4 47.7 58.4 25.6 38.8 57.2 27.4 18.8 32.3 9.5 4.2 9.9 14.7 2.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1	81.6 87.8 82.9 48.4 13.7 4.2 21.5 36.7 69.4 57.2 8.1 12.4 41.5 48.4 43.0 18.8 - 9.9 24.0 52.2 11.2 - 9.9 - 4.2 - - - - - - - - - - - - -	81.0 79.1 55.2 9.9 - 2.8 17.1 38.8 45.7 38.8 8.1 - 4.2 11.2 31.0 29.6 14.7 - 6.2 9.9 17.1 11.2 - - - - - - - - - - - - - - - - - - -	34.6 25.6 11.2 - 14.7 13.7 21.5 8.1 9.9 13.7 - - - - - - - - - - - - - - - - - - -	17.1 6.2	

Table IX. Test levels of the mass points VJ, pseudo-standardized normal samples, N = 20,  $t_c = 0,.125,.250,.375,1.0$ Mass points not appearing is this table have a TL<1%

v <sub>1</sub>	<b>v</b> <sub>2</sub> <b>v</b> <sub>3</sub>	0	1	2	3	4	5	6	7	8	9
0	0	52.9	94.6	90.0	76.0	58.3	35.7	20.1	5.7	1.6	
0	1	56.1	97.0	100.0	92.2	74.3	49.9	21.7	9.0	4.6	_
0	2	41.7	68.3	85.6	87.7	65.6	41.7	15.6	9.9	4.6	_
0	1 2 3 4 5 6	15.6	46.3	55.0	60.6	41.7	31.7	17.8	4.0	4.6	1.6
0	4	7.8	33.4	32.8	30.7	25.0	13.2	4.6	1.6	2.4	_
0	5	4.0	13.8	13.8	13.2	10.6	8.1	3.2	-		_
0	6	2.4	5.7	6.3	_	3.2	-	1.6	_	_	_
0	7	-	2.4	3.2	-	_		-	_	_	_
0	7	-	-	-	1.6	-	_	-	_	_	_
1	0	28.4	49.0	64.3	54.0	38.3	28.4	13.2	5.7	3.2	2.4
1	1	27.5	71.2	83.6	77.8	66.9	43.9	22.0	7.8	4.6	4
1	2	35.7	63.0	81.5	79.6	72.7	37.6	21.0	7.8	6.3	1.6
1	1 2 3 4 5 6	21.0	47.2	69.8	59.5	44.7	23.5	14.9	9.9	1.6	_
1	4	9.9	32.8	37.0	35.7	25.8	13.2	7.8	3.2	_	_
1	5	4.0	13.8	22.8	16.8	15.6	6.3	4.0	-	_	_
1	6	1.6	5.7	13.2	8.1	3.2	3.2	-	_	_	_
1	7	-	2.4	4.0	4.0	_	_	_	-	_	_
1	9	-	-	-	-	1.6	_	_	_	_	_
2	0	7.8	24.6	36.3	26.2	24.6	10.3	11.0	2.4	1.6	_
2	1 2	14.4	46.3	50.9	61.8	43.2	20.1	16.1	7.8	3.2	_
2	2	20.1	39.6	51.9	57.2	39.6	22.8	16.1	7.8	2.4	_
2	3	14.9	29.3	42.4	48.0	31.2	14.4	9.0	4.0	-	_
2	4	6.3	21.0	30.7	28.8	17.8	9.9	8.1	1.6	-	_
2	5	2.4	7.8	10.3	13.2	11.3	5.7	3.2	-	1.6	_
2	6	2.4	3.2	9.9	7.8	4.0	1.6	_	_	_	_
2 2 2 2 2 2 2 2	7	-	-	3.2	-		-	_	_	_	_
2	8	-	-	-	1.6	-	-	-	-	_	_

Table IX (Continued)

Table X. Test levels of the mass points VJ, pseudo-standardized Weibull samples,  $\alpha = 0.1$ , N = 20,  $t_c = 0$ ; .125; .250; .375; 1.0 Mass points not appearing in this table have a TL 1%

		pornus		appeari		41110	00010	navo a	TL 19
$v_1$ $v_2$	0	1	2	3	4	5	6	7	8
0 0 1 2 3 4 5 6 0 1 2 3 4 5 6 0 1 2 3 4 5 0 1 2 3 4 5 5 6 0 1 2 3 3 3 3 3 3 4 4 4 4 5 5 5 6 0 1 2 3 4 5 6 0 1 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	93.3 72.9 41.2 18.1 7.8 2.0 45.9 38.4 22.5 10.4 5.6 2.0 17.8 17.6 11.8 6.3 2.3 4.4 6.3 4.4 2.3 1.0 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6	100.0 87.2 63.9 34.8 12.7 4.4 1.0 69.6 66.7 47.5 25.6 12.7 4.4 1.0 29.8 33.7 27.2 15.0 7.4 10.4 9.8 2.8 1.0 1.6 2.8 5.1 2.0	81.9 77.1 55.9 31.7 14.4 4.8 1.6 51.5 61.2 49.3 24.8 32.6 24.8 32.6 32	58.5 44.3 21.8	30.7 37.1 21.0 11.8 6.3 1.0 23.2 28.0 19.8 11.2 3.4 16.7 13.4 10.4 4.4 - 3.7 6.3 7.3 3.4	14.7 16.3 14.4 5.1 3.4 1.0 8.8 15.4 10.4 5.6 1.0 1.6 1.6 1.6 1.6	4.8 3.7 2.0 1.6 - 3.4 7.3 2.0 1.6 - - 2.8 3.4 2.8 2.8	2.0 1.6 - 1.0 - 2.0 1.0 - - - - - -	1.0

### Tests of the hypothesis that the distributions of Table XI.

### VJR and VJS are identical for equal class

### probabilities

a) R = pseudo-standardized exponential population

S = -"- normal N = 10, r = 4,  $p_i = 1/r = 25\%$ 

		S S	ign	test	Nr-of-r	uns test	R	ank-sur	n test
	Nr. of pairs		.of		Nr.of runs	Reject.	T <sub>1</sub>	<sup>T</sup> 2	Reject.
8000	4	1	1	-	2	-	18.0	18.0	55.7
0017	12	4	6	> 25	7	88.1	136.0	164.0	21.8
0026	12	1	11	= 1	3	-	129.5	170.5	12.3
0035	12	4	5	> 25	5	50.0	144.5	155.5	38.7
0044	6	0	6	= 10	0	-	31.0	47.0	12.0
0116	12	2	10	= 5	3	18.2	139.0	161.0	
0125	24	13	11	> 25	9	7.5	604.5	571.5	
0134	24	10	14	> 25	8 5 5	3.7	582.0	594.0	45.9
0224	12	6	6	> 25	5	17.5	149.0	151.0	
0233	12	3	8	= 25	5	53.3	140.0	160.0	
1115	4	2	2	> 25	4	> 90.0	15.5	20.5	
1124	12	7	5	> 25	6	42.4	148.5	151.5	
1133	6	4	2	> 25	3	40.0	34.0	34.0	24.2
1223	12	9	3	= 25	4	20.0	184.5	115.5	2.5

b) R = pseudo-standardized Weibull,  $\alpha = 1.0$ , population S = -"- Weibull,  $\alpha = 0.1$ , -"-

N = 10, r = 4,  $p_i = 1/r = 25\%$ 

Types Nr. of Pairs   Nr. of Reject.   Nr. of Reject.   T1   T2   Reject.      0008			Si	gn ·	test	Nr-of-m	uns test	R	ank-sur	n test
0017       12       1       8       =       5       3       -       127.5       172.5       10.0         0026       12       3       6       > 25       3       10.7       144.0       156.0       37.5         0035       12       4       8       > 25       7       78.8       143.0       157.0       35.5         0044       6       4       2       > 25       4       80.0       40.5       37.5       43.9         0116       12       5       7       > 25       6       42.4       133.0       167.0       17.0         0125       24       12       12       > 25       9       7.2       583.5       582.5       46.0         0134       24       12       12       > 25       13       50.0       582.0       594.0       45.9         0224       12       7       5       > 25       4       7.6       152.5       147.5       45.4         0233       12       7       5       > 25       7       65.2       154.0       146.0       42.1         115       4       3       1       > 25       2       -			Nr.		Reject.	The second second	1 1	-1_		%
1133 6 4 2 > 25 3 40.0 42.0 36.0 35.0	0017 0026 0035 0044 0116 0125 0134 0224 0233 1115 1124	12 12 12 6 12 24 24 12 12	0 1 3 4 4 5	682712125517	= 25 5 25 > 25 > 25 > 25 > 25 > 25 > 25 >	0 3 3 7 4 6 9	10.7 78.8 80.0 42.4 7.2 50.0 7.6 65.2	127.5 144.0 143.0 40.5 133.0 583.5 582.0 152.5 154.0 20.5	20.5 172.5 156.0 157.0 37.5 167.0 582.5 594.0 147.5 146.0 15.5	10.0 37.5 35.5 43.9 17.0 46.0 45.9 45.4 42.1 29.3

Table XII. Test levels of the mass points VJ, pseudo-standar-dized variables, N = 10, r = 4, p = 1/r = 25%

Mass	TL Mass	TL	Mass	т	Mass	m <sub>T</sub>
points	points		points	$\mathbf{T}$ L	points	$\mathbf{TL}$
	% No VJ	%	No VJ	%	No VJ	%
	.2 43 0703		84 2024	29.0	125 3302	35.3
	.1 44 0710		85 2033	36.1	126 3311	71.8
	4 45 0800		86 2042	25.5	127 3320	54.9
4 0035 11	.8   46 1007		87 2051	6.3	128 3401	15.8
	.8 47 1016		88 2060	0.0	129 3410	34.5
	• 3   48 1025 • 4   49 1034		89 2105	10.4	130 3500	6.1
	.2   50 1043		90 2114 91 2123	51.3	131 4004	0.7
	.0   51 1052			79.5	132 4013	7.4
	.8   52 1061		93 2141	85.6	133 4022	19.6
The state of the s	.5   53 1070		94 2150	47.8 3.7	134 4031 135 4040	13.3
12 0125 33	.0 54 1106		95 2204	20.7	136 4103	2.1 11.4
13 0134 40	.1   55 1115		96 2213	73.7	137 4112	53.7
14 0143 31			97 2222	100.0	138 4121	57.3
15 0152 13		70.0		87.8	139 4130	24.9
16 0161 2	.5   58 1142	57.3	99 2240	22.7	140 4202	23.2
	.0   59 1151	18.6	100 2303	27.8	141 4211	68.3
18 0206 2	.6 60 1160		101 2312	83.5	142 4220	41.3
19 0215 26			102 2321	90.0	143 4301	28.4
20 0224 44			103 2330	43.6	144 4310	46.7
21 0233 58			104 2402	19.6	145 4400	6.8
22 0242 37			105 2411	52.5	146 5003	1.3
23 0251 11, 24 0260 0,			106 2420	38.8	147 5012	5.8
	.4   66 1250 .3   67 1304		107 2501	8.5	148 5021	5.3
26 0314 21	.1   68 1313		108 2510	16.2	149 5030	3.2
27 0323 42		83.5	109 2600 110 3005	2.1	150 5102	4.2
28 0332 37		68.3	110 3005 111 3014	1.4	151 5111	34.5
29 0341 14	8 71 1340	17.6	112 3023	9.5	152 5120 153 5201	16.7
30 0350 3.		10.8	113 3032	30.3	154 5210	14.9
31 0404 2		39.7	114 3041	12.9	155 5300	33.0 12.2
32 0413 14.		64.0	115 3050	1.0	156 6002	1.3
33 0422 29.		24.9	116 3104	10.4	157 6011	1.7
34 0431 22.		7.7	117 3113	50.2	158 6020	2.5
35 0440 2.		21.6	118 3122	75.6	159 6101	3.8
36 0503 0.	7 78 1520	8.2	119 3131	59.9	160 6110	8.8
37 0512 4.	7 79 1601	1.7	120 3140	15.3	161 6200	5.1
38 0521 5.		3.5	121 3203	26.6	162 7001	0.5
39 0530 1.		0.1	122 3212	77.6	163 7010	0.3
40 0602 0.		0.6	123 3221	92.2	164 7100	1.7
41 0611 2.		12.9	124 3230	45.7	165 8000	0.1
42 0620 1.	0	-			-	-

Table XIII. Percentiles of pseudo-standardized variables for N = 10, N = 20, and various distribution functions

N = 10

P	1.0	0.9	0.7	0.5	0.3	0.1	Normal dbn
0.0	.0000	.0000	.0000	.0000	.0000	.0000	.0000
12.5	.0435	.0542	.0824	.1220	.1725	.2323	.1810
25.0	.0938	.1123	.1585	.2189	.2933	. 3780	.3035
37.5	.1542	.1786	.2373	.3104	. 3957	.4904	. 4055
50.0	.2280	.2570	.3233	.4025	.4913	-5853	.5000
62.5	.3197	.3511	.4212	. 4998	.5857	.6732	•5945
75.0	.4461	.4772	.5443	.6160	.6900	.7635	.6965
87.5	.6377	.6625	.7126	.7640	.8151	.8635	.8190
100.0	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000

N = 20

βα	1.0	0.9	0.7	0.5	0.3	0.1	Normal dbn
0.0	.000	.000	.000	.000	.000	.000	.000
12.5	.030	.040	.079	.130	.192	.278	.205
25.0	.075	.095	.145	.217	.310	.416	.322
37.5	.130	.155	.215	.300	.405	.518	.416
50.0	.194	.220	.294	.384	.492	.605	.502
62.5	.268	.304	.382	.475	•577	.680	•585
75.0	.382	.418	.492	.580	.671	.762	.678
87.5	.560	.590	.660	.722	.790	.857	•795
100.0	1.000	1.000	1.000	1.000	1.000	1.000	1.000

Table XI The effect of pooling on the decision power of VJ

Stage	Nr.of	Decision power in %					
of pooling	points	1 vs 0.1	1 vs 0	0.1 vs 0			
VJ, ungrouped	165	77.2	69.1	22.0			
Types of VJ	15	18.4	6.6	21.6			
x <sup>2</sup>	14	18.4	6.6	21.6			
NE	4	13.0	5.6	13.6			

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The test statistic X <sup>2</sup> of the Chi-squa be used for selecting distribution functi purpose its decision power was found to be inherent property of its definition. In o statistic, denoted by VJ, was introduced, elements which fall within each of r property of the variable x has been divided. In factobalized from VJ by a pooling procedure, much larger decision power than X <sup>2</sup> as was power for a specified case being 6.6% for The properties of VJ have been thoroug limits yielding the largest decision power in some cases, the decision power was foundationed.  The statistic VJ can also be used for is acceptable or not and also for selecting such distributions. Necessary tables for	ons. When exe very small rder to elim It is defined of X <sup>2</sup> may be For this reaverified by X <sup>2</sup> was rais hly exmanine r have been and to be som stating whether the most	amining it due to a inate this ed by the classes i regarded son VJ was the examp ed to 69.1 d. In part determined ewhat larg her a hypo propable o	s use for this kind of pooling, an pooling, a new test number v, of sample nto which the space as a statistic expected to have a le that the decision % for VJ. icular the class with the result that, er than anyone sofar thetical distribution ne within a set of			

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